

Computational fracture mechanics with **SAMCEF**

New trends and illustration on an industrial test case

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NAFEMS Nordic Regional Conference, "Trends and Future Needs in Engineering Simulation", Gothenburg, Sweden, 26-27 October, 2010

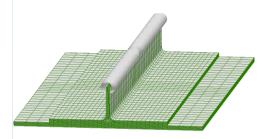
Few words about SAMTECH

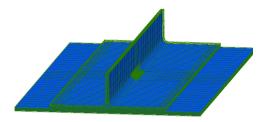


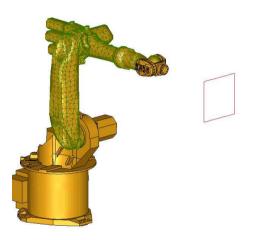
Composite and aeronautics applications

Delamination in a composite structures

Flexible systems dynamics and mechatronics







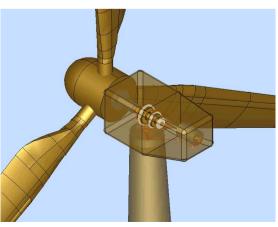
SAMCEF Finite Element code

Bird impact on a leading edge structure. Contact within the structure

Bird impact on a slat

Courtesy of SONACA

Wind turbine modelling



Few words about SAMTECH











































































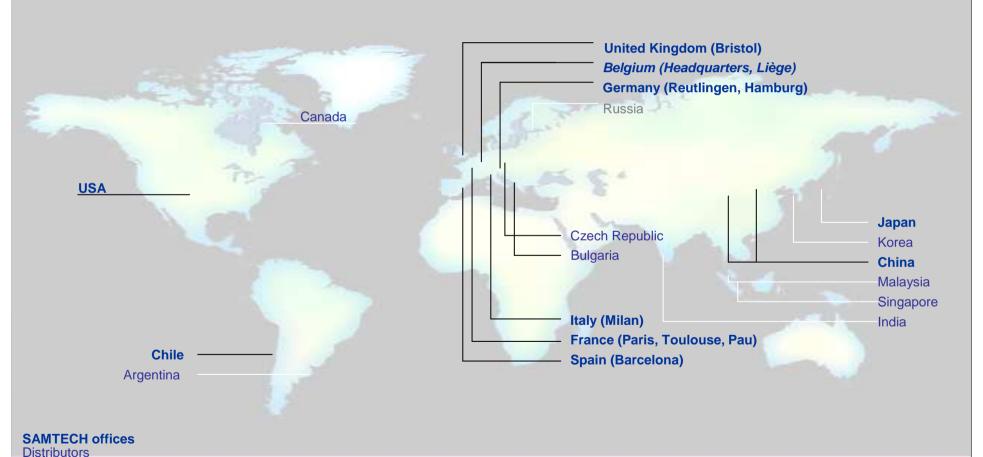




Few words about SAMTECH



World wide representation



Outline



- Methods available in SAMCEF for fracture mechanics
- XFEM method in SAMCEF
- Applications of XFEM with SAMCEF
- Conclusions

...let me recall that SAMCEF has been used for more than 25 years by the largest aerospace companies in Europe

...SAMCEF is already selected for its XFEM solution by :







Methods available in SAMCEF



	FEM with crack box	FEM without crack box	XFEM
2D			
3D			

Outline



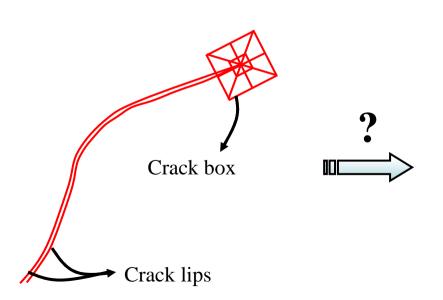
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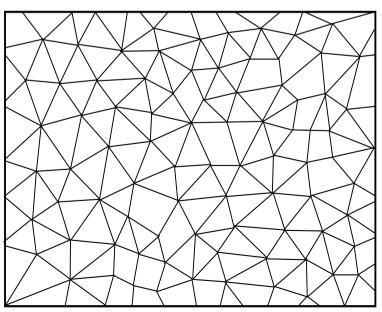
Why XFEM method?



Classic FE approach

- Difficulty to include a crack in an existing mesh
 - => define new geometric items (crack lips) + define a crack box around the crack tip
- Difficulty to study a crack propagation
 - => modification of the geometry
 - => remeshing is required at each step

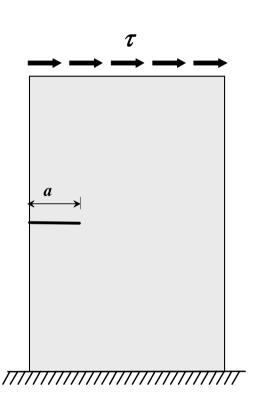




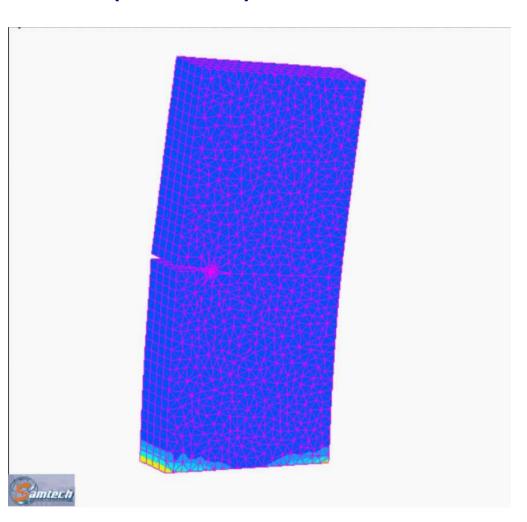
Classic FE method: illustration



Crack propagation with bifurcation (crack box)





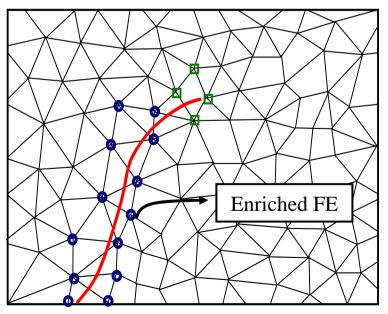


Advantages of XFEM method

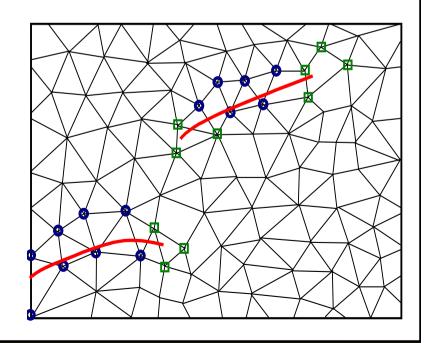


XFEM approach: easier definition of a crack

- A crack can be easily defined in the structure
- The crack is defined on the mesh, and can cut the elements
- No more crack box (the stress singularity is included in the enrichment)
- A same mesh can be used to study different crack configurations



OR

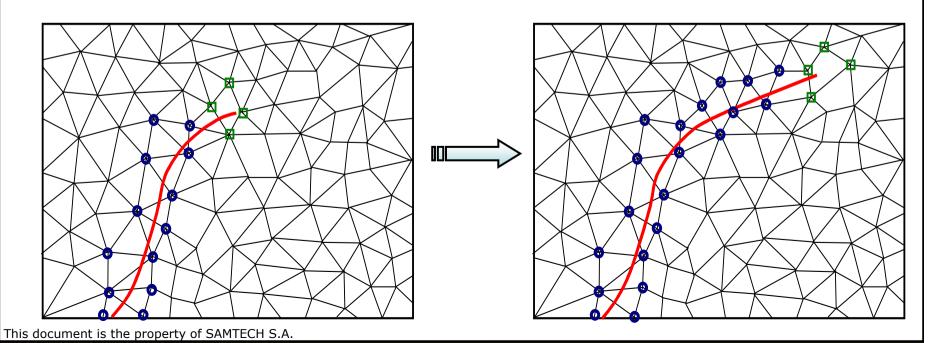


Advantages of XFEM method



XFEM approach: simplified crack propagation

- The crack is defined on the mesh, and can cut the elements
- No more crack box to move with the crack tip
- No more updating of the geometry (crack tips)
- => no remeshing (to some extent)



XFEM method features in SAMCEF



XFEM in SAMCEF

Enrichment (true XFEM method of Belytschko and Moes)
 Specific integration scheme is adpoted
 Implicit crack representation with level-sets
 Stress Intensity Factors (SIF) computation
 Automatic fatigue crack propagation
 Research contacts and partnerships

- Prof. Nicolas Moës (Ecole Centrale de Nantes, France)

- CENAERO (Belgium): our key partner



XFEM method: enrichment

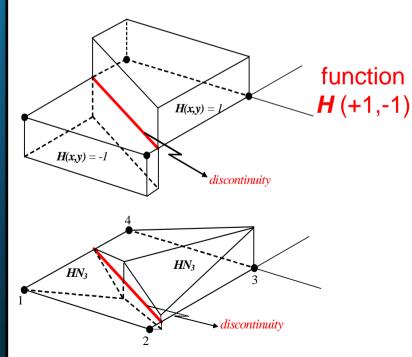


$$u(\mathbf{x}) = \sum_{i \in N} u_i N_i(\mathbf{x}) + \sum_{i \in L} b_i N_i(\mathbf{x}) H(\mathbf{x}) + \sum_{i \in K_1} N_i(\mathbf{x}) \left(\sum_{l=1}^4 F_l(\mathbf{x}) c_i^l \right)$$

Classical dof

Additional dof

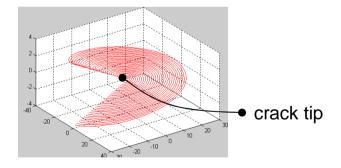
Displacement discontinuity



Crack tip

• discontinuity of u(x) $F_1(x) = \sqrt{r} \sin(\theta/2)$

$$F_1(\mathbf{x}) = \sqrt{r} \sin(\theta / 2)$$



accuracy of the solution

$$F_1(\mathbf{x}) = \sqrt{r} \sin(\theta/2)$$
 $F_3(\mathbf{x}) = \sqrt{r} \sin(\theta/2) \sin(\theta)$

$$F_2(\mathbf{x}) = \sqrt{r}\cos(\theta/2)$$
 $F_4(\mathbf{x}) = \sqrt{r}\cos(\theta/2)\sin(\theta)$

XFEM method: integration

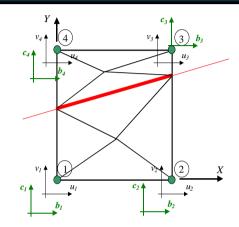


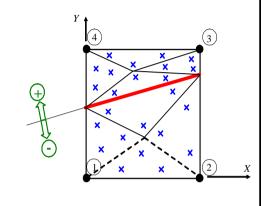
Integration (2D elements)

Element cut by the crack



Triangulation of the element for the integration





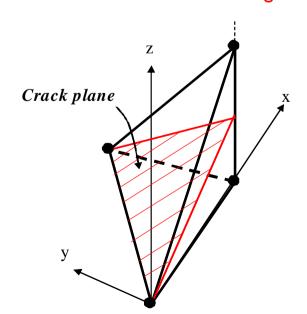
Discontinuous H function => integration on each side

Integration (3D elements)

Element cut by the crack



Division of the element for the integration



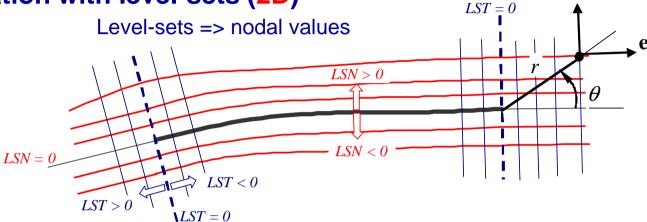
XFEM method: crack representation



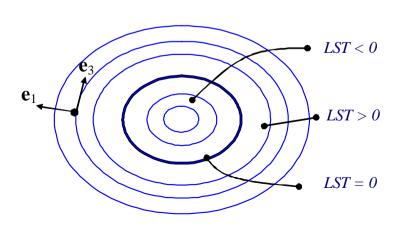
Implicit representation with level-sets (2D)

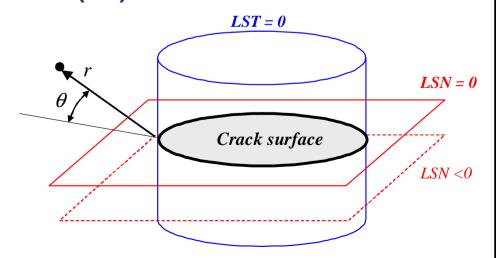
$$r = \sqrt{LSN^2 + LST^2}$$

$$\theta = tg^{-1} \frac{LSN}{LST}$$



Implicit representation with level-sets (3D)





XFEM method: SIF computation



Computation of the Stress Intensity Factors K_1 and K_2 (2D)

Interaction integral

(variant of the J integral on an equivalent domain)

$$J = J^{(1)} + J^{(2)} + I^{(1,2)}$$

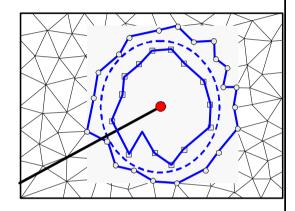
- (1) Present state
- (2) Auxiliary state

$$I^{(1,2)} = -\int_{A} \theta_{m,j} (\sigma_{kl}^{(1)} \varepsilon_{kl}^{(2)} \delta_{mj} - \sigma_{ij}^{1} u_{i,m}^{(2)} - \sigma_{ij}^{(2)} u_{i,m}^{(1)}) dA$$

$$I^{(1,2)} = \frac{2(1-v^2)}{E} \left(K_I^{(1)} K_I^{(2)} + K_{II}^{(1)} K_{II}^{(2)} \right) => K_I \text{ for } K_I^{(2)} = 1 \text{ and } K_{II}^{(2)} = 0$$

$$=> K_I \text{ for } K_I^{(2)} = 1 \text{ and } K_{II}^{(2)} = 0$$

$$=> K_{II} \text{ for } K_I^{(2)} = 0 \text{ and } K_{II}^{(2)} = 1$$



Computation of the Stress Intensity Factors K₁, K₂ and K₃ (3D)

Crack front

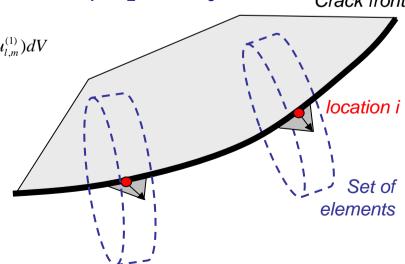
Interaction integral

(variant of the J integral on an equivalent domain)

$$I_{i}^{(1,2)} = -\int_{A} \theta_{m,j} (\sigma_{kl}^{(1)} \varepsilon_{kl}^{(2)} \delta_{mj} - \sigma_{lj}^{1} u_{l,m}^{(2)} - \sigma_{lj}^{(2)} u_{l,m}^{(1)}) dV$$

$$I_i^{(1,2)} = G_i^{(1,2)} \int_{\Gamma_i} \theta ds$$

$$G^{(1,2)} = \frac{2(1-v^2)}{E} \left(K_I^{(1)} K_I^{(2)} + K_{II}^{(1)} K_{II}^{(2)} \right) + \frac{1}{\mu} K_{III}^{(1)} K_{III}^{(2)}$$



XFEM method: crack propagation



For 2D problems (available since 2005 in SAMCEF)

- Not automatic
- Iterative process managed by the user
- Possibility to use BOSS quattro, with a parameterized BACON bank file
- Level-sets completely re-initialized at each iteration

For 3D problems

- Automatic
- Based on the update of the level-sets (Δa , θ)
- Criterion = maximum principal stress
- Fatigue based on the Paris/Nasgro law

Bifurcation angle

$$\theta^p = 2 \arctan \left(\frac{K_I \pm \sqrt{K_I^2 + 8K_{II}^2}}{4K_{II}} \right)$$

Propagation / fatigue

$$\frac{da}{dN} = C\left(\Delta K_I^{eff}\right)^m \qquad \Delta a = \Delta a^{\max} \left(\frac{\Delta K_I^{eff}}{\Delta K_{\text{Im}\,ax}^{eff}}\right)^m$$

$$\Delta K_{I}^{eff} = fct \left(\Delta K_{I}, \Delta K_{II}, \Delta K_{III}, \theta^{p}, material \right)$$

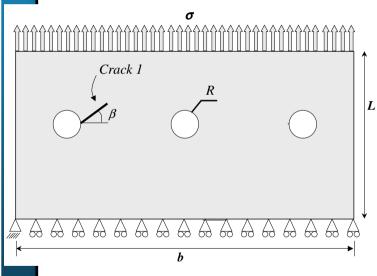
Outline

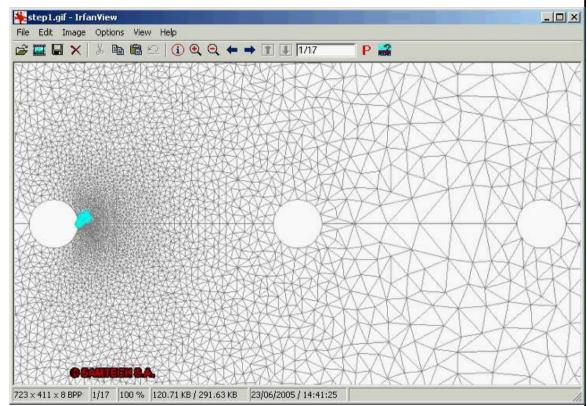


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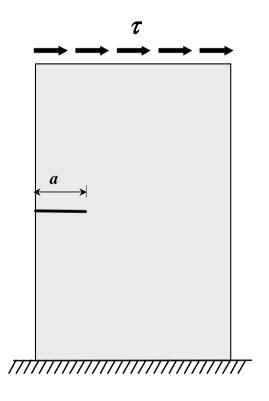
2D Propagation (done in 2005 for **GAIRBUS**)



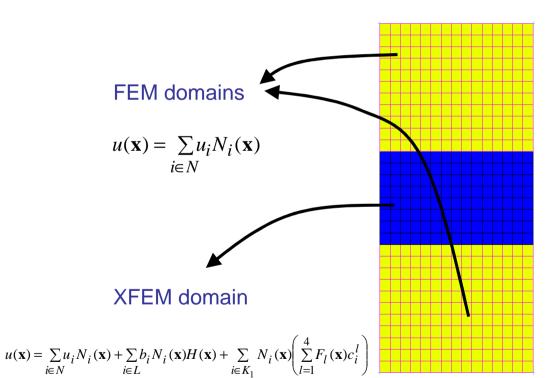




Classical benchmark (3D)

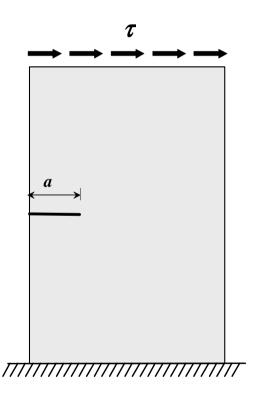


Initial finite element mesh

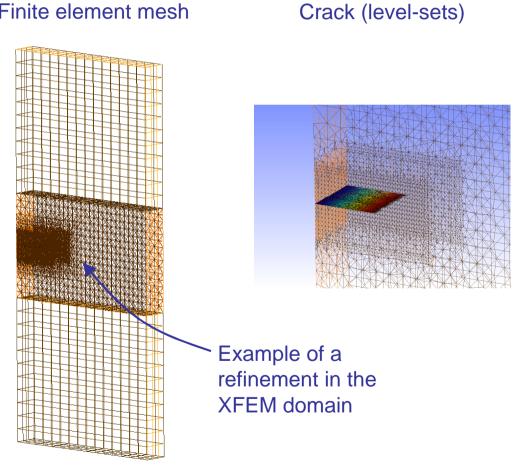




Classical benchmark (3D)



Finite element mesh

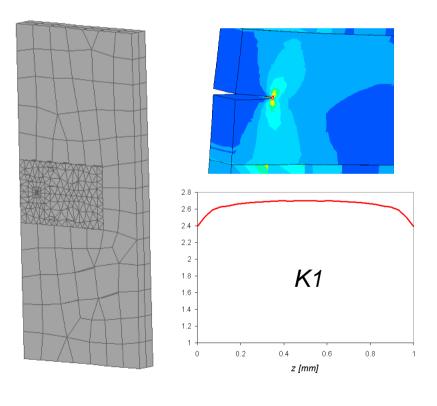


No remeshing during the crack propagation

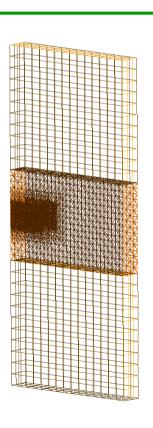


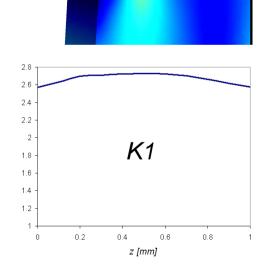
Classical benchmark (3D)

FEM (crack box)



XFEM (level-sets)



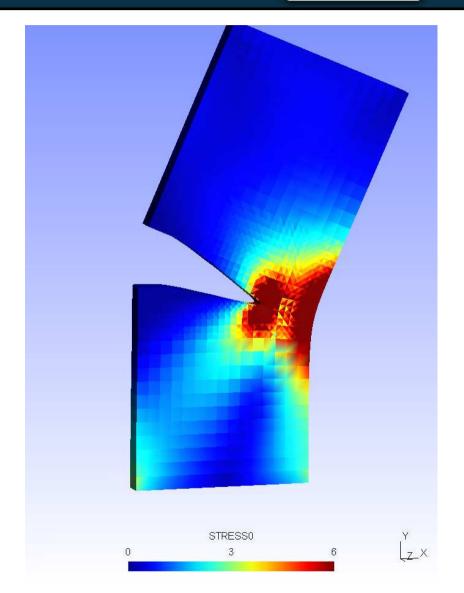




Classical benchmark (3D)

3D propagation

Bifurcation



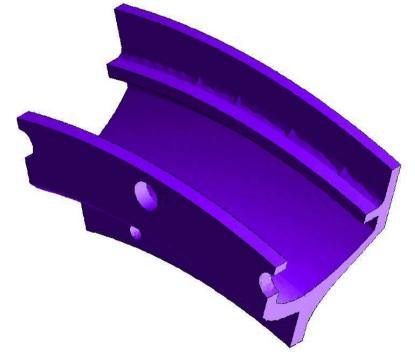


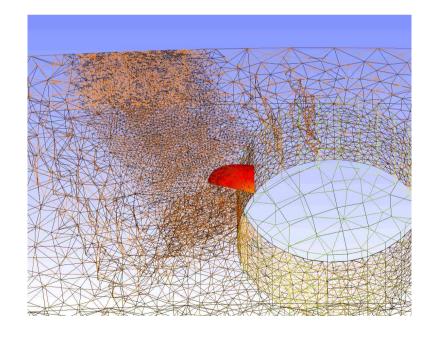
Industrial test case

Centrifugal load
Imposed radial displacement

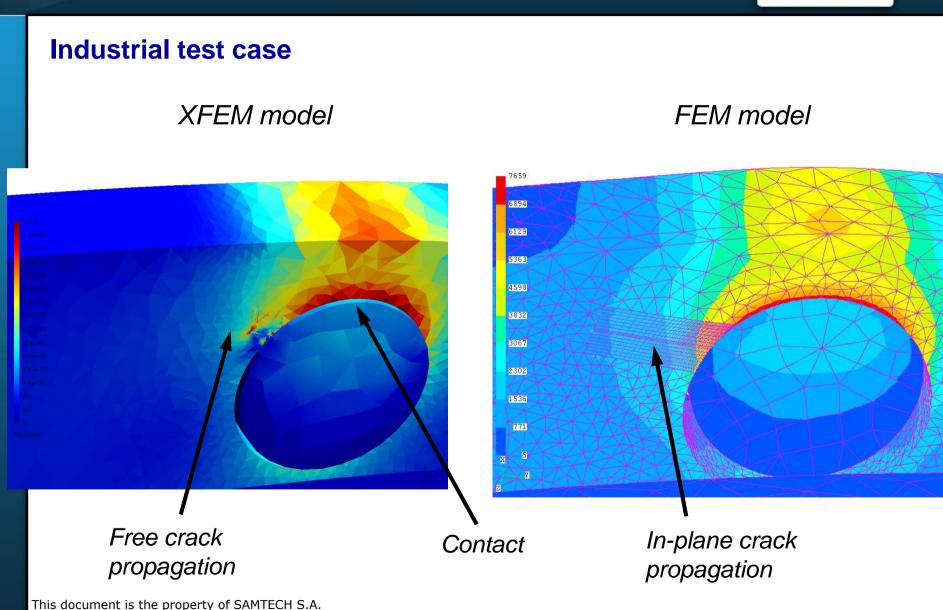
Location of the crack (1/4 of a circle)

Level-sets

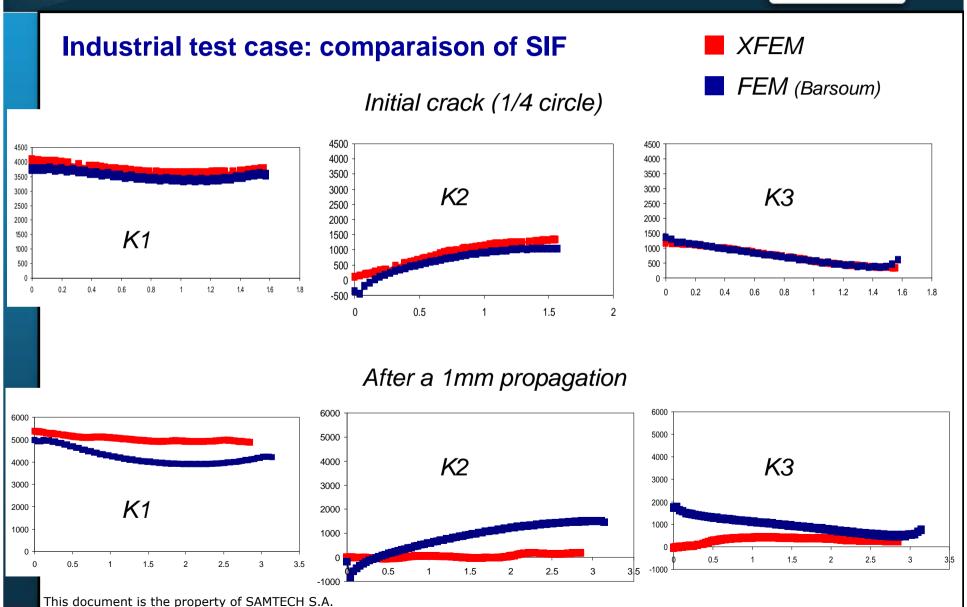








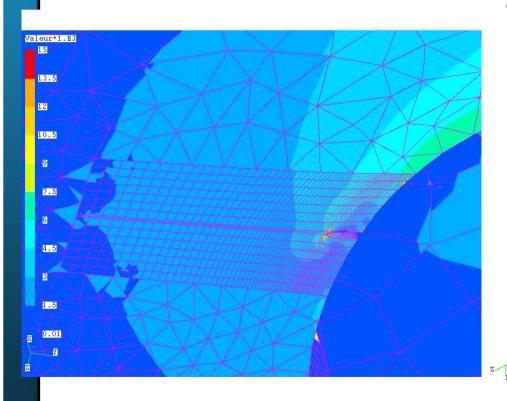


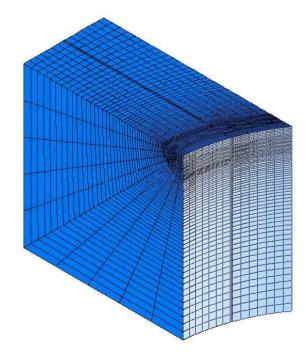




Industrial test case: FEM and Barsoum elements

Elliptical cack propagation in a plane
Parameterized model with a crack box

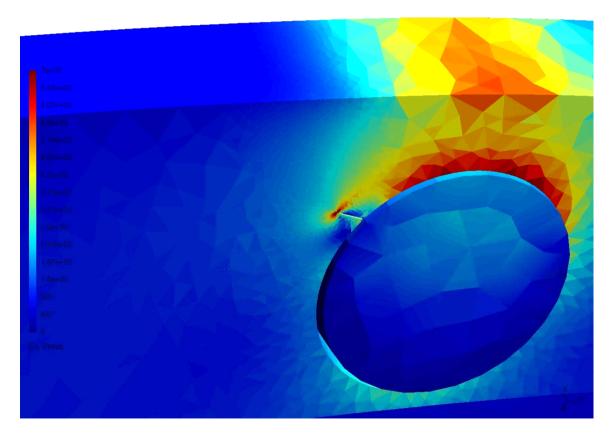






Industrial test case: XFEM (initial crack of 1mm)

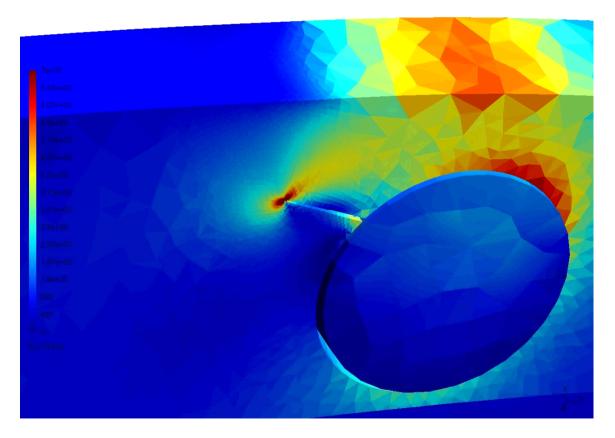
Free crack propagation, with bifurcation





Industrial test case: XFEM (initial crack of 3mm)

Free crack propagation, with bifurcation



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Conclusions



- TFEM is a powerful method for fracture mechanics
- XFEM simplifies the life of the analyst for fracture mechanics problems
- ** XFEM available in SAMCEF for 2D and 3D fracture mechanics problems
 - Crack modelled in a very simple way
 - Automatic crack propagation (3D problems)
- ** XFEM in SAMCEF is still under improvements for/with our industrial partners
- XFEM is a easy, ready and the best solution for fracture mechanics



Thank you

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